

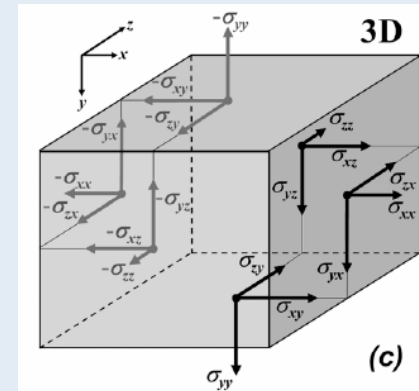
# **Numerical Modelling in Geosciences**

**Lecture 6  
Deformation**

# Tensor

Second-rank tensor  $\rightarrow$  stress (  $\sigma$  ), strain (  $\varepsilon$  ), strain rate (  $\dot{\varepsilon}$  )

$$\sigma_{ij} = \begin{bmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} \end{bmatrix}$$



Invariants (quantities independent of the coordinate system):

- First invariant  $\rightarrow$  trace:  $tr(\sigma_{ij}) = (\sigma_{xx} + \sigma_{yy} + \sigma_{zz})$

- Second invariant  $\rightarrow$  magnitude:

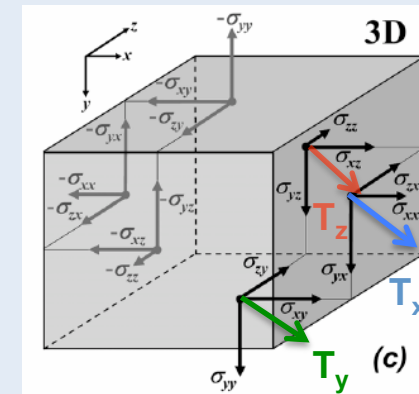
$$\|\sigma\| = \sqrt{\frac{1}{2} \sigma_{ij}^2} = \sqrt{\frac{1}{2} (\sigma_{xx}^2 + \sigma_{xy}^2 + \sigma_{xz}^2 + \sigma_{yx}^2 + \sigma_{yy}^2 + \sigma_{yz}^2 + \sigma_{zx}^2 + \sigma_{zy}^2 + \sigma_{zz}^2)}$$

- Third invariant  $\rightarrow$  determinant

# Stress

In geodynamics compressional (extensional) stress are negative (positive). Pressure is positive under compression. Stress is measured in Pa = N/m<sup>2</sup>. The stress tensor contains the components of the tractions acting on the element surfaces. The first index indicate the direction of stress, the second the normal to the stressed surface

$$\sigma_{ij} = \begin{bmatrix} \sigma_{xx} & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} \end{bmatrix}$$



Pressure is equal to the mean normal stress:

$$2D: P = -\frac{tr(\sigma)}{2} = -\frac{\sigma_{kk}}{2} = -\frac{\sigma_{xx} + \sigma_{yy}}{2}$$

$$3D: P = -\frac{tr(\sigma)}{3} = -\frac{\sigma_{kk}}{3} = -\frac{\sigma_{xx} + \sigma_{yy} + \sigma_{zz}}{3}$$

In absence of internal angular momentum, the tensor is symmetric:

$$\sigma_{xy} = \sigma_{yx}$$

$$\sigma_{xz} = \sigma_{zx}$$

$$\sigma_{zy} = \sigma_{yz}$$

# Deviatoric Stress

Stress can be divided into a deviatoric and an isotropic components. The deviatoric components produce flow, the isotropic components (i.e., pressure) compaction/dilation.

$$\sigma_{ij} = \sigma'_{ij} + \delta_{ij} \frac{\sigma_{kk}}{3} = \sigma'_{ij} - P\delta_{ij} \quad \text{where} \quad \delta_{ij} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix};$$

$$3D: \sigma'_{ij} = \begin{bmatrix} \sigma'_{xx} & \sigma'_{xy} & \sigma'_{xz} \\ \sigma'_{yx} & \sigma'_{yy} & \sigma'_{yz} \\ \sigma'_{zx} & \sigma'_{zy} & \sigma'_{zz} \end{bmatrix} = \begin{bmatrix} \sigma_{xx} + P & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} + P & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} + P \end{bmatrix}$$

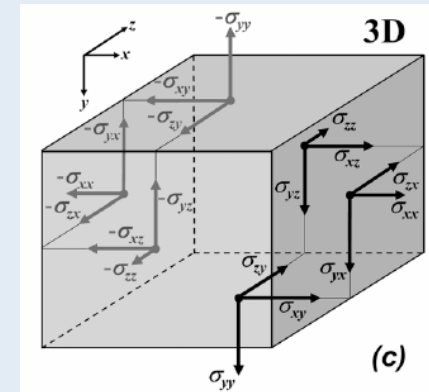
Normal deviatoric stress:  $\sigma'_{ii} = \sigma_{ii} + P$ ;

Shear deviatoric stress:  $\sigma'_{ij} = \sigma'_{ji} = \sigma_{ij} = \sigma_{ji}$

Please, show that  $tr(\sigma'_{ij}) = 0$

Second invariant of deviatoric stress tensor:

$$\sigma'_{II} = \sqrt{\frac{1}{2} \sigma'_{ij}{}^2} = \sqrt{\frac{1}{2} (\sigma'_{xx}{}^2 + \sigma'_{yy}{}^2 + \sigma'_{zz}{}^2) + \sigma'_{xy}{}^2 + \sigma'_{xz}{}^2 + \sigma'_{yz}{}^2}$$



# Deviatoric Stress

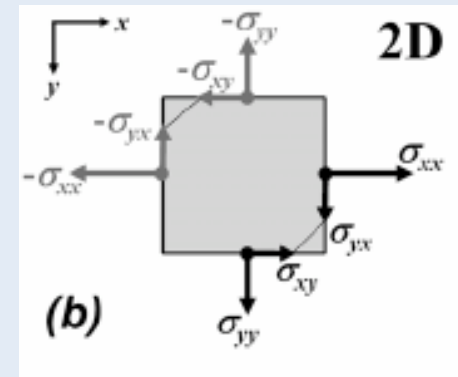
Stress can be divided into a deviatoric and an isotropic components. The deviatoric components produce flow, the isotropic component (i.e., pressure) compaction/dilation

$$2D: \sigma'_{ij} = \begin{bmatrix} \sigma'_{xx} & \sigma'_{xy} \\ \sigma'_{yx} & \sigma'_{yy} \end{bmatrix} = \begin{bmatrix} \sigma_{xx} + P & \sigma_{xy} \\ \sigma_{yx} & \sigma_{yy} + P \end{bmatrix}$$

*Please, show that in 2D  $\Rightarrow \sigma'_{xx} = -\sigma'_{yy}$*

*Second invariant of deviatoric stress tensor :*

$$\sigma'_{II} = \sqrt{\frac{1}{2} \sigma'_{ij}{}^2} = \sqrt{\sigma'_{xx}{}^2 + \sigma'_{xy}{}^2}$$



# Tectonic pressure

If a medium is at rest, then no deviatoric stresses exist and the total pressure is equal to the lithostatic pressure.

$$P_{TOT} = P_{LITH} = P_0 + g \int_0^z \rho(z) dz$$

When deformation is applied, the total pressure is equal to the lithostatic pressure + the tectonic pressure

$$P_{TOT} = P_{LITH} + P_{TECT}$$

$$P_{TECT} = -\frac{\sigma_{kk}}{3} - P_{LITH}$$

Exercise:

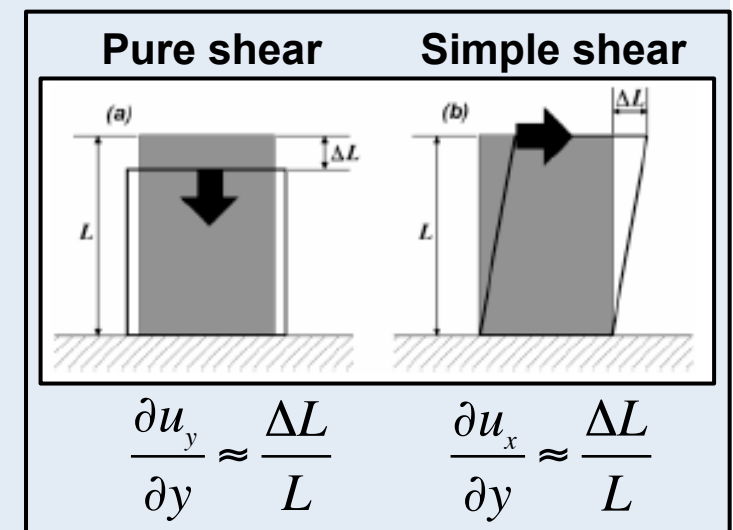
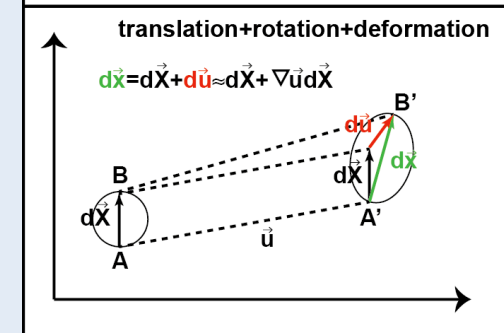
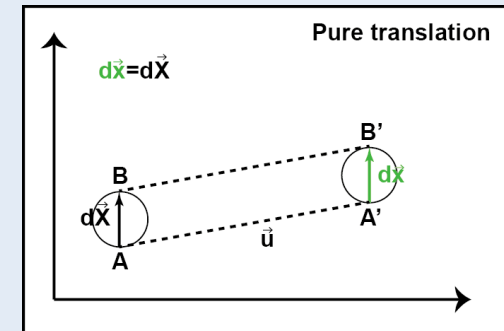
Calculate the lithostatic, total and tectonic pressures, and the total and deviatoric stress tensors at 10 km depth in the crust (density = 2500 kg/m<sup>3</sup>, g<sub>z</sub>=10 m/s<sup>2</sup>), when a compressional stress of 150 MPa is applied along the x direction.

# Displacement, its gradient and velocity

$$\text{Displacement : } \vec{u} = \begin{bmatrix} u_x \\ u_y \\ u_z \end{bmatrix}$$

$$\text{Rate of displacement : } \frac{D\vec{u}}{Dt} = \vec{v} = \begin{bmatrix} v_x \\ v_y \\ v_z \end{bmatrix}$$

$$\text{Displacement gradient : } \nabla \vec{u} = \frac{\partial u_i}{\partial j} = \begin{bmatrix} \frac{\partial u_x}{\partial x} & \frac{\partial u_x}{\partial y} & \frac{\partial u_x}{\partial z} \\ \frac{\partial u_y}{\partial x} & \frac{\partial u_y}{\partial y} & \frac{\partial u_y}{\partial z} \\ \frac{\partial u_z}{\partial x} & \frac{\partial u_z}{\partial y} & \frac{\partial u_z}{\partial z} \end{bmatrix}$$



# Displacement gradient, strain, rotation

Displacement gradient (adimensional)= Strain (symmetric) + Rotation (anti-symmetric)

$$\nabla \vec{u} = \frac{\partial u_i}{\partial j} = \begin{bmatrix} \frac{\partial u_x}{\partial x} & \frac{\partial u_x}{\partial y} & \frac{\partial u_x}{\partial z} \\ \frac{\partial u_y}{\partial x} & \frac{\partial u_y}{\partial y} & \frac{\partial u_y}{\partial z} \\ \frac{\partial u_z}{\partial x} & \frac{\partial u_z}{\partial y} & \frac{\partial u_z}{\partial z} \end{bmatrix}$$

$$\nabla \vec{u} = \frac{1}{2}(\nabla \vec{u} + \nabla \vec{u}^T) + \frac{1}{2}(\nabla \vec{u} - \nabla \vec{u}^T) = \frac{1}{2}\left(\frac{\partial u_i}{\partial j} + \frac{\partial u_j}{\partial i}\right) + \frac{1}{2}\left(\frac{\partial u_i}{\partial j} - \frac{\partial u_j}{\partial i}\right)$$

$$\varepsilon_{ij} = \frac{1}{2}\left(\frac{\partial u_i}{\partial j} + \frac{\partial u_j}{\partial i}\right) \quad (\text{Strain})$$

$$\omega_{ij} = \frac{1}{2}\left(\frac{\partial u_i}{\partial j} - \frac{\partial u_j}{\partial i}\right) \quad (\text{Rotation})$$

$$\nabla \vec{u} = \varepsilon + \omega$$

$$\nabla \vec{u} = \begin{bmatrix} \frac{\partial u_x}{\partial x} & \frac{1}{2}\left(\frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x}\right) & \frac{1}{2}\left(\frac{\partial u_x}{\partial z} + \frac{\partial u_z}{\partial x}\right) \\ \frac{1}{2}\left(\frac{\partial u_y}{\partial x} + \frac{\partial u_x}{\partial y}\right) & \frac{\partial u_y}{\partial y} & \frac{1}{2}\left(\frac{\partial u_y}{\partial z} + \frac{\partial u_z}{\partial y}\right) \\ \frac{1}{2}\left(\frac{\partial u_z}{\partial x} + \frac{\partial u_x}{\partial z}\right) & \frac{1}{2}\left(\frac{\partial u_z}{\partial y} + \frac{\partial u_y}{\partial z}\right) & \frac{\partial u_z}{\partial z} \end{bmatrix} + \begin{bmatrix} 0 & \frac{1}{2}\left(\frac{\partial u_x}{\partial y} - \frac{\partial u_y}{\partial x}\right) & \frac{1}{2}\left(\frac{\partial u_x}{\partial z} - \frac{\partial u_z}{\partial x}\right) \\ \frac{1}{2}\left(\frac{\partial u_y}{\partial x} - \frac{\partial u_x}{\partial y}\right) & 0 & \frac{1}{2}\left(\frac{\partial u_y}{\partial z} - \frac{\partial u_z}{\partial y}\right) \\ \frac{1}{2}\left(\frac{\partial u_z}{\partial x} - \frac{\partial u_x}{\partial z}\right) & \frac{1}{2}\left(\frac{\partial u_z}{\partial y} - \frac{\partial u_y}{\partial z}\right) & 0 \end{bmatrix}$$



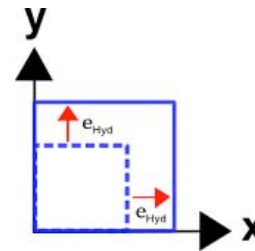
# Strain

Indicates the amount of deformation and is adimensional

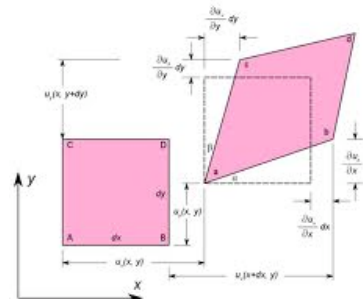
$$\varepsilon_{ij} = \frac{1}{2} \left( \frac{\partial u_i}{\partial j} + \frac{\partial u_j}{\partial i} \right) = \begin{bmatrix} \frac{\partial u_x}{\partial x} & \frac{1}{2} \left( \frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x} \right) & \frac{1}{2} \left( \frac{\partial u_x}{\partial z} + \frac{\partial u_z}{\partial x} \right) \\ \frac{1}{2} \left( \frac{\partial u_y}{\partial x} + \frac{\partial u_x}{\partial y} \right) & \frac{\partial u_y}{\partial y} & \frac{1}{2} \left( \frac{\partial u_y}{\partial z} + \frac{\partial u_z}{\partial y} \right) \\ \frac{1}{2} \left( \frac{\partial u_z}{\partial x} + \frac{\partial u_x}{\partial z} \right) & \frac{1}{2} \left( \frac{\partial u_z}{\partial y} + \frac{\partial u_y}{\partial z} \right) & \frac{\partial u_z}{\partial z} \end{bmatrix}$$

*Volumetric strain* =  $\Delta V = tr(\varepsilon_{ij}) = \varepsilon_{kk} = \varepsilon_{11} + \varepsilon_{22} + \varepsilon_{33}$

*If incompressible*  $\Rightarrow \Delta V = tr(\varepsilon_{ij}) = \nabla \cdot \vec{u} = 0$



*Deviatoric strain* :  $\varepsilon'_{ij} = \varepsilon_{ij} - \frac{1}{3} \delta_{ij} \varepsilon_{kk}$



# Velocity gradient, strain rate, vorticity

Velocity gradient (s<sup>-1</sup>)= Strain rate (symmetric) + Vorticity (anti-symmetric)

$$\nabla \vec{v} = \frac{\partial v_i}{\partial j} = \begin{bmatrix} \frac{\partial v_x}{\partial x} & \frac{\partial v_x}{\partial y} & \frac{\partial v_x}{\partial z} \\ \frac{\partial v_y}{\partial x} & \frac{\partial v_y}{\partial y} & \frac{\partial v_y}{\partial z} \\ \frac{\partial v_z}{\partial x} & \frac{\partial v_z}{\partial y} & \frac{\partial v_z}{\partial z} \end{bmatrix}$$

$$\nabla \vec{v} = \frac{1}{2}(\nabla \vec{v} + \nabla \vec{v}^T) + \frac{1}{2}(\nabla \vec{v} - \nabla \vec{v}^T) = \frac{1}{2} \left( \frac{\partial v_i}{\partial j} + \frac{\partial v_j}{\partial i} \right) + \frac{1}{2} \left( \frac{\partial v_i}{\partial j} - \frac{\partial v_j}{\partial i} \right)$$

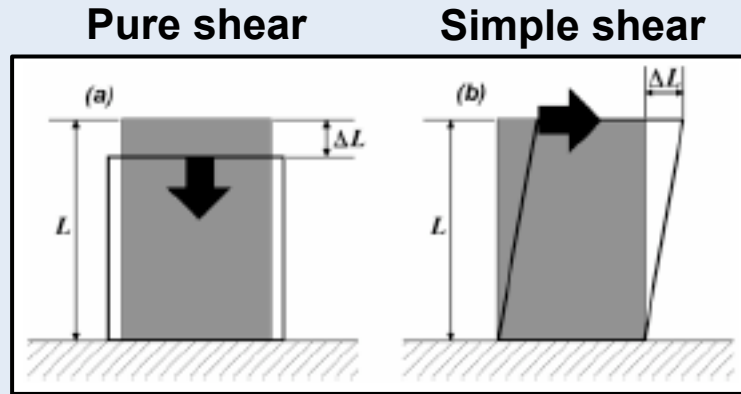
$$\dot{\epsilon}_{ij} = \frac{1}{2} \left( \frac{\partial v_i}{\partial j} + \frac{\partial v_j}{\partial i} \right) \quad (\text{Strain rate})$$

$$\dot{\omega}_{ij} = \frac{1}{2} \left( \frac{\partial v_i}{\partial j} - \frac{\partial v_j}{\partial i} \right) \quad (\text{Vorticity, rotation rate})$$

$$\nabla \vec{v} = \dot{\epsilon} + \dot{\omega}$$

$$\nabla \vec{v} = \begin{bmatrix} \frac{\partial v_x}{\partial x} & \frac{1}{2} \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) & \frac{1}{2} \left( \frac{\partial v_x}{\partial z} + \frac{\partial v_z}{\partial x} \right) \\ \frac{1}{2} \left( \frac{\partial v_y}{\partial x} + \frac{\partial v_x}{\partial y} \right) & \frac{\partial v_y}{\partial y} & \frac{1}{2} \left( \frac{\partial v_y}{\partial z} + \frac{\partial v_z}{\partial y} \right) \\ \frac{1}{2} \left( \frac{\partial v_z}{\partial x} + \frac{\partial v_x}{\partial z} \right) & \frac{1}{2} \left( \frac{\partial v_z}{\partial y} + \frac{\partial v_y}{\partial z} \right) & \frac{\partial v_z}{\partial z} \end{bmatrix} + \begin{bmatrix} 0 & \frac{1}{2} \left( \frac{\partial v_x}{\partial y} - \frac{\partial v_y}{\partial x} \right) & \frac{1}{2} \left( \frac{\partial v_x}{\partial z} - \frac{\partial v_z}{\partial x} \right) \\ \frac{1}{2} \left( \frac{\partial v_y}{\partial x} - \frac{\partial v_x}{\partial y} \right) & 0 & \frac{1}{2} \left( \frac{\partial v_y}{\partial z} - \frac{\partial v_z}{\partial y} \right) \\ \frac{1}{2} \left( \frac{\partial v_z}{\partial x} - \frac{\partial v_x}{\partial z} \right) & \frac{1}{2} \left( \frac{\partial v_z}{\partial y} - \frac{\partial v_y}{\partial z} \right) & 0 \end{bmatrix}$$

# End-member flows



$$\text{Pure Shear: } \nabla \vec{v} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 0 \end{bmatrix} = \dot{\epsilon} + \dot{\omega} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 0 \end{bmatrix} + \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\text{Simple Shear: } \nabla \vec{v} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} = \dot{\epsilon} + \dot{\omega} = \begin{bmatrix} 0 & \frac{1}{2} & 0 \\ \frac{1}{2} & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} + \begin{bmatrix} 0 & \frac{1}{2} & 0 \\ -\frac{1}{2} & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

# Strain rate

The strain rate tensor can be divided into a deviatoric and isotropic components. Dimension is (s<sup>-1</sup>).  
The trace of the strain rate tensor gives the rate of volume change

$$\dot{\epsilon}_{ij} = \begin{bmatrix} \dot{\epsilon}_{xx} & \dot{\epsilon}_{xy} & \dot{\epsilon}_{xz} \\ \dot{\epsilon}_{yx} & \dot{\epsilon}_{yy} & \dot{\epsilon}_{yz} \\ \dot{\epsilon}_{zx} & \dot{\epsilon}_{zy} & \dot{\epsilon}_{zz} \end{bmatrix} = \frac{1}{2} \left( \frac{\partial v_i}{\partial j} + \frac{\partial v_j}{\partial i} \right) = \begin{bmatrix} \frac{\partial v_x}{\partial x} & \frac{1}{2} \left( \frac{\partial v_x}{\partial y} + \frac{\partial v_y}{\partial x} \right) & \frac{1}{2} \left( \frac{\partial v_x}{\partial z} + \frac{\partial v_z}{\partial x} \right) \\ \frac{1}{2} \left( \frac{\partial v_y}{\partial x} + \frac{\partial v_x}{\partial y} \right) & \frac{\partial v_y}{\partial y} & \frac{1}{2} \left( \frac{\partial v_y}{\partial z} + \frac{\partial v_z}{\partial y} \right) \\ \frac{1}{2} \left( \frac{\partial v_z}{\partial x} + \frac{\partial v_x}{\partial z} \right) & \frac{1}{2} \left( \frac{\partial v_z}{\partial y} + \frac{\partial v_y}{\partial z} \right) & \frac{\partial v_z}{\partial z} \end{bmatrix}$$

$$\dot{\epsilon}_{ij} = \dot{\epsilon}'_{ij} + \frac{1}{3} \dot{\epsilon}_{kk} \delta_{ij}$$

$$tr(\dot{\epsilon}_{ij}) = \dot{\epsilon}_{kk} = \dot{\epsilon}_{11} + \dot{\epsilon}_{22} + \dot{\epsilon}_{33} = \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial z} = \nabla \cdot \vec{v} = \Delta \dot{V}$$

If incompressible  $\Rightarrow \Delta \dot{V} = tr(\dot{\epsilon}_{ij}) = \nabla \cdot \vec{v} = 0$

$$tr(\dot{\epsilon}'_{ij}) = 0$$

Second invariant of deviatoric strain rate tensor :  $\dot{\epsilon}'_{II} = \sqrt{\frac{1}{2} \dot{\epsilon}'_{ij}{}^2}$

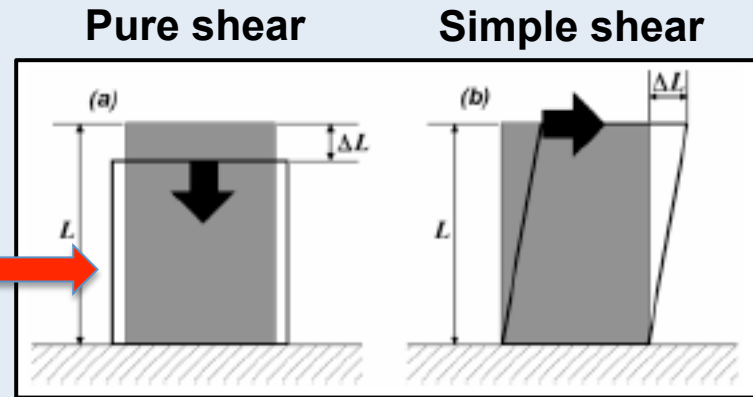
$\dot{\epsilon}_{xy} = \dot{\epsilon}_{yx} = \dot{\epsilon}'_{xy} = \dot{\epsilon}'_{yx}$
$\dot{\epsilon}_{xz} = \dot{\epsilon}_{zx} = \dot{\epsilon}'_{xz} = \dot{\epsilon}'_{zx}$
$\dot{\epsilon}_{zy} = \dot{\epsilon}_{yz} = \dot{\epsilon}'_{zy} = \dot{\epsilon}'_{yz}$

# Displacement vs deformation gradient

Displacement gradient

$$\nabla \vec{u} = \frac{\partial u_i}{\partial j} = \begin{bmatrix} \frac{\partial u_x}{\partial x} & \frac{\partial u_x}{\partial y} & \frac{\partial u_x}{\partial z} \\ \frac{\partial u_y}{\partial x} & \frac{\partial u_y}{\partial y} & \frac{\partial u_y}{\partial z} \\ \frac{\partial u_z}{\partial x} & \frac{\partial u_z}{\partial y} & \frac{\partial u_z}{\partial z} \end{bmatrix} \Rightarrow \frac{\partial u_y}{\partial y} = \frac{\Delta L}{L}$$

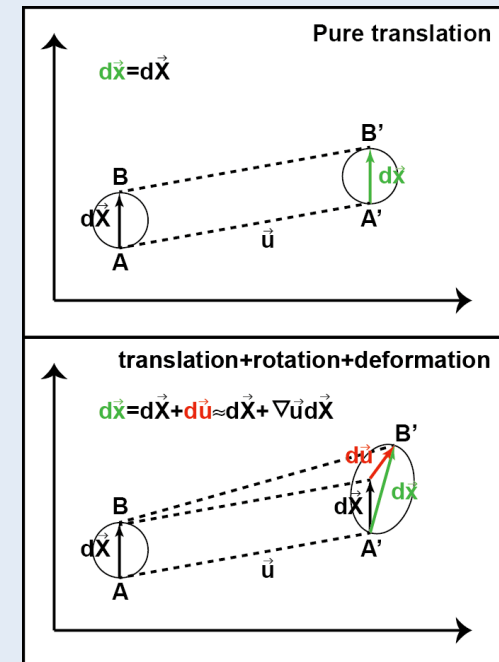
Length variation over the initial length



Deformation gradient

$$F_{ij} = I + \nabla \vec{u} = \delta_{ij} + \frac{\partial u_i}{\partial j} = \begin{bmatrix} 1 + \frac{\partial u_x}{\partial x} & \frac{\partial u_x}{\partial y} & \frac{\partial u_x}{\partial z} \\ \frac{\partial u_y}{\partial x} & 1 + \frac{\partial u_y}{\partial y} & \frac{\partial u_y}{\partial z} \\ \frac{\partial u_z}{\partial x} & \frac{\partial u_z}{\partial y} & 1 + \frac{\partial u_z}{\partial z} \end{bmatrix} \Rightarrow F_{yy} = \frac{L + \Delta L}{L} = 1 + \frac{\partial u_y}{\partial y}$$

Final length over the initial length



# Time derivative of deformation gradient

We can track the history of deformation for a given Lagrangian particle by computing the time derivative of  $F$ , and successively by isolating the amount of deformation from the amount of rotation.

For homogeneous, steady-state flow:

$$\frac{\partial F}{\partial t} = \nabla \vec{v} \cdot F \Rightarrow F^{t+\Delta t} = F^t + \nabla \vec{v} \cdot F \cdot \Delta t$$

*Left stretch tensor* :  $B = F \cdot F^T$

Initial  
deformation  
gradient

$$F_{ij}^{t=0} = \delta_{ij} = I = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

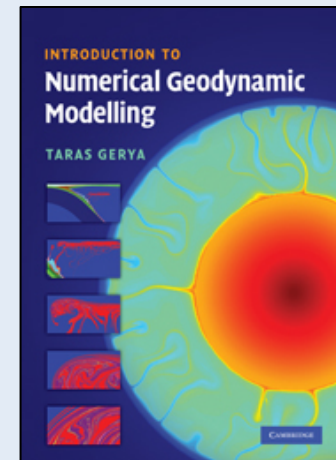
Eigenvalues and eigenvectors of  $B$  give, respectively, the square of the magnitude and orientation of the principal stretch axes.

Time to practice...

# Homework

**Read chapter 4 of textbook:**

Gerya, T. *Introduction to numerical geodynamic modelling*.  
Cambridge University Press, 345 pp. (2010)



**Practice with code we have built to track the deformation history**